

ELEC 5530/6530
Robot Control
Lecture 5: Robot Dynamics:
Structure and Properties of the Robot Equation

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Motivation:

The controller is simpler and more effective if the known properties of the arm are incorporated in the design stage.

Robot Arm Model with friction and disturbances

$$M(q)\ddot{q} + V(q, \dot{q}) + \underline{F(\dot{q})} + \underline{G(q)} + \underline{\tau_d} = \tau,$$

with q the joint variable n -vector and τ the n -vector of generalized forces. $M(q)$ is the inertia matrix, $V(q, \dot{q})$ the Coriolis/centripetal vector, and $G(q)$ the gravity vector. We have added a friction term

$$F(\dot{q}) = \underline{F_v \dot{q}} + F_d$$

with F_v the coefficient matrix of viscous friction and F_d a dynamic friction term. Also added is a disturbance τ_d , which could represent, for instance, any inaccurately modeled dynamics.

$$M(q)\ddot{q} + \underline{N(q, \dot{q})} + \underline{\tau_d} = \tau,$$

where

$$N(q, \dot{q}) \equiv V(q, \dot{q}) + F(\dot{q}) + G(q)$$

represents nonlinear terms.

TABLE 2.3-1 The Robot Equation and Its Properties

$$M(q)\ddot{q} + V(q, \dot{q}) + F(\dot{q}) + G(q) + \tau_d = \tau$$

or

$$M(q)\ddot{q} + N(q, \dot{q}) + \tau_d = \tau$$

where

$$N(q, \dot{q}) = V(q, \dot{q}) + F(\dot{q}) + G(q)$$

Inertia Matrix:

$M(q)$ is symmetric and positive definite.

$$\mu_1 I \leq M(q) \leq \mu_2 I$$

$$m_1 \leq \|M(q)\| \leq m_2$$

Coriolis/Centripetal Vector:

$V(q, \dot{q})$ is quadratic in $\dot{q}$

$$\|V(q, \dot{q})\| \leq v_b \|\dot{q}\|^2$$

$$V(q, \dot{q}) = V_m(q, \dot{q})\dot{q}$$

$S(q, \dot{q}) = \dot{M}(q) - 2V_m(q, \dot{q})$ is a skew-symmetric matrix.

Friction Terms:

$$F(\dot{q}) = F_v \dot{q} + F_d(\dot{q})$$

$$F_v = \text{diag}\{v_i\}$$

$$F_d(\dot{q}) = K_d \text{sgn}(\dot{q}), \text{ with } K_d = \text{diag}\{k_i\}$$

$$\|F_v \dot{q} + F_d(\dot{q})\| \leq v \|\dot{q}\| + k$$

Gravity Vector:

$$\|G(q)\| \leq g_b$$

Disturbance Term:

$$\|\tau_d\| \leq d$$

Linearity in the Parameters:

$$M(q)\ddot{q} + V(q, \dot{q}) + F_v \dot{q} + F_d(\dot{q}) + G(q)$$

$$= M(q)\ddot{q} + N(q, \dot{q}) = W(q, \dot{q}, \ddot{q})\phi$$

one norm ✓

$$\| \cdot \|_1$$

$$\begin{bmatrix} v_1 & 0 & \dots & 0 \\ 0 & v_2 & & \\ \vdots & & \ddots & \\ 0 & & & v_n \end{bmatrix}$$

$\text{sgn}(\dot{q})$

$$\begin{array}{c} \sqrt{} \\ -1 \quad 0 \\ \hline 0 \quad 1 \\ \hline \end{array} \dot{q}$$

$$\begin{bmatrix} k_1 & & & \\ & k_2 & & \\ & & \ddots & \\ & & & k_n \end{bmatrix}$$

$$\text{sgn}(\dot{q}) = \begin{cases} -1, & \text{if } \dot{q} < 0 \\ 0, & \text{if } \dot{q} = 0 \\ 1, & \text{if } \dot{q} > 0 \end{cases}$$

Example 1. Structure and Bounds for Two-Link Planar Arm Model

$$\begin{bmatrix} (m_1 + m_2) a_1^2 + m_2 a_2^2 + 2m_2 a_1 a_2 \cos \theta_2 & m_2 a_2^2 + m_2 a_1 a_2 \cos \theta_2 \\ m_2 a_2^2 + m_2 a_1 a_2 \cos \theta_2 & m_2 a_2^2 \end{bmatrix} \begin{bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{bmatrix} + \begin{bmatrix} -m_2 a_1 a_2 (2\dot{\theta}_1 \dot{\theta}_2 + \dot{\theta}_2^2) \sin \theta_2 \\ m_2 a_1 a_2 \dot{\theta}_1^2 \sin \theta_2 \end{bmatrix} + \begin{bmatrix} (m_1 + m_2) g a_1 \cos \theta_1 + m_2 g a_2 \cos (\theta_1 + \theta_2) \\ m_2 g a_2 \cos (\theta_1 + \theta_2) \end{bmatrix} = \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix}.$$

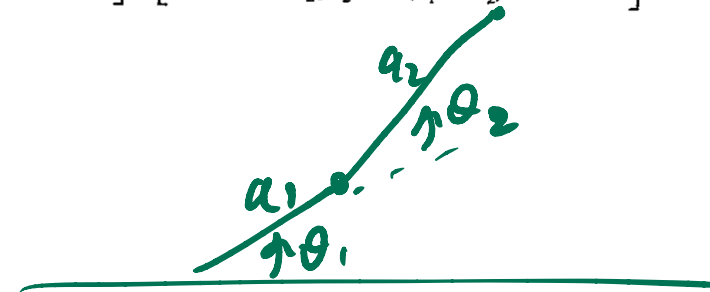
These manipulator dynamics are in the standard form

$$\underline{M(q)} \ddot{q} + \underline{V(q, \dot{q})} + \underline{G(q)} = \underline{\tau},$$

$$\underline{M(q)} = \begin{bmatrix} \overset{M_{11}}{(m_1 + m_2) a_1^2 + m_2 a_2^2 + 2m_2 a_1 a_2 \cos \theta_2} & \overset{M_{12}}{m_2 a_2^2 + m_2 a_1 a_2 \cos \theta_2} \\ \overset{M_{21}}{m_2 a_2^2 + m_2 a_1 a_2 \cos \theta_2} & \overset{M_{22}}{m_2 a_2^2} \end{bmatrix}$$

$$\underline{V(q, \dot{q})} = \begin{bmatrix} \overset{V_1}{-m_2 a_1 a_2 (2\dot{\theta}_1 \dot{\theta}_2 + \dot{\theta}_2^2) \sin \theta_2} \\ \overset{V_2}{m_2 a_1 a_2 \dot{\theta}_1^2 \sin \theta_2} \end{bmatrix}$$

$$\underline{G(q)} = \begin{bmatrix} (m_1 + m_2) g a_1 \cos \theta_1 + m_2 g a_2 \cos (\theta_1 + \theta_2) \\ m_2 g a_2 \cos (\theta_1 + \theta_2) \end{bmatrix}.$$



1 norm of vector

$\| \cdot \|_1 \rightarrow$ one norm

$$x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}$$

$$\|x\|_1 = \sum_{i=1}^n |x_i|$$

exp.

$$x = \begin{bmatrix} 1 \\ 0 \\ 2 \end{bmatrix}$$

$$\|x\|_1 = 1 + 0 + 2 = 3$$

1 norm of matrix

$$X = \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1n} \\ \vdots & & & \\ x_{n1} & x_{n2} & \dots & x_{nn} \end{bmatrix} \equiv [x_{ij}]$$

$$\|X\|_1 = \max_{1 \leq j \leq n} \sum_{i=1}^n |a_{ij}|$$

$$= \max \{ |x_{11}| + |x_{21}| + \dots + |x_{n1}|$$

⋮

$$|x_{1n}| + |x_{2n}| + \dots + |x_{nn}| \}$$

$$X = \begin{bmatrix} -3 & -5 & 7 \\ 2 & 6 & 4 \\ 0 & 2 & 8 \end{bmatrix},$$

$$\|X\|_1 = \max \{ \begin{array}{l} | -3 | + | 2 | + | 0 | \\ | -5 | + | 6 | + | 2 | \\ | 7 | + | 4 | + | 8 | \end{array} \}$$

a. Bounds on the Intertia Matrix

$$= 19$$

$$\|M(q)\|_1 = \max \{ |M_{11}| + |M_{21}|, |M_{12}| + |M_{22}| \}$$

Due to $|a+b| \leq |a| + |b|$,

$$|M_{11}| \leq (m_1 + m_2)a_1^2 + m_2 a_2^2 + 2m_2 a_1 a_2 \triangleq a$$

$$|M_{21}| \leq m_2 a_2^2 + m_2 a_1 a_2 \triangleq b$$

$$\frac{|m_2 a_1^2 - m_1 a_1 a_2|}{+ m_2 a_2^2} \|M(q)\|_1 \leq a + b$$

b. Bounds on the Centripetal Term

$$\|V\|_1 = |V_1| + |V_2|$$

$$|V_1| \leq m_2 a_1 a_2 (2|\dot{\theta}_1 \dot{\theta}_2| + \dot{\theta}_2^2)$$

$$|V_2| \leq m_2 a_1 a_2 \dot{\theta}_1^2$$

$$\begin{aligned} |V_1| + |V_2| &\leq m_2 a_1 a_2 \left(\dot{\theta}_1^2 + 2|\dot{\theta}_1 \dot{\theta}_2| + \dot{\theta}_2^2 \right) \\ &\leq m_2 a_1 a_2 \left(\dot{\theta}_1 + \dot{\theta}_2 \right)^2 \end{aligned}$$

c. Bounds on the Friction Term

$$F(\dot{q}) = F_v \dot{q} + F_d$$

$$F_v = \text{diag}[v_i]$$

$$F_d = K_d \text{sgn}(\dot{q}), \quad K_d = \text{diag}[k_i]$$


$$\begin{bmatrix} |v_1| & & \\ & |v_2| & \\ & & \ddots \\ & & & |v_n| \end{bmatrix}$$

$$\|F(\dot{q})\|_1 \leq \underbrace{\|F_v \dot{q}\|_1} + \underbrace{\|F_d\|_1}$$

$$\leq |v_{\max}| |\dot{q}| + |k_{\max}|$$

d. Bounds on the Gravity and Disturbance Terms

$$G(q) = \begin{pmatrix} (m_1 + m_2)g a_1 \cos \theta_1 + m_2 g a_2 \cos(\theta_1 + \theta_2) \\ m_2 g a_2 \cos(\theta_1 + \theta_2) \end{pmatrix}$$

$$\begin{aligned} \|G(q)\|_1 &= |(m_1 + m_2)g a_1 \cos \theta_1 + m_2 g a_2 \cos(\theta_1 + \theta_2)| \\ &\quad + |m_2 g a_2 \cos(\theta_1 + \theta_2)| \\ &\leq |(m_1 + m_2)g a_1 \cos \theta_1| + |m_2 g a_2 \cos(\theta_1 + \theta_2)| \\ &\quad + |m_2 g a_2 \cos(\theta_1 + \theta_2)| \leq (m_1 + m_2)g a_1 + m_2 g a_2 + m_2 g a_2 \end{aligned}$$

e. The Robot Function Parameter Matrix W

$$\tau_1 = [(m_1 + m_2)a_1^2 + m_2a_2^2 + 2m_2a_1a_2 \cos \theta_2]\ddot{\theta}_1 + [m_2a_2^2 + m_2a_1a_2 \cos \theta_2]\ddot{\theta}_2 \\ - m_2a_1a_2(2\dot{\theta}_1\dot{\theta}_2 + \dot{\theta}_2^2) \sin \theta_2 + (m_1 + m_2)ga_1 \cos \theta_1 + m_2ga_2 \cos (\theta_1 + \theta_2) \\ + v_1\dot{\theta}_1 + k_1 \operatorname{sgn}(\dot{\theta}_1)$$

$$\tau_2 = [m_2a_2^2 + m_2a_1a_2 \cos \theta_2]\ddot{\theta}_1 + m_2a_2^2\ddot{\theta}_2 + m_2a_1a_2\dot{\theta}_1^2 \sin \theta_2 \\ + m_2ga_2 \cos (\theta_1 + \theta_2) + v_2\dot{\theta}_2 + k_2 \operatorname{sgn}(\dot{\theta}_2).$$

$$\tau_{2 \times 1} = W_{2 \times 6} \varphi_{6 \times 1}, \text{ where } \varphi = \begin{bmatrix} m_1 \\ m_2 \\ k_1 \\ k_2 \\ v_1 \\ v_2 \end{bmatrix}$$

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} w_{11} & w_{12} & w_{13} & w_{14} & w_{15} & w_{16} \\ w_{21} & w_{22} & w_{23} & w_{24} & w_{25} & w_{26} \end{bmatrix} \begin{bmatrix} m_1 \\ m_2 \\ k_1 \\ k_2 \\ v_1 \\ v_2 \end{bmatrix}_{6 \times 1}$$

$$w_{11} = a_1^2 \ddot{\theta}_1 + \theta a_1 \cos \theta_1$$

$$w_{12} = (a_2^2 + a_1^2 + 2a_1a_2 \cos \theta_2) \ddot{\theta}_1 + (a_2^2 + a_1a_2 \cos \theta_2) \ddot{\theta}_2$$

$$w_{13} = \operatorname{sgn}(\dot{\theta}_1)$$

$$w_{14} = 0$$

$$w_{15} = \dot{\theta}_1$$

$$w_{16} = 0$$

$$w_{21} = 0$$

$$\begin{aligned} w_{22} = & a_2^2 \ddot{\theta}_1 + a_1 a_2 \cos \theta_2 \ddot{\theta}_1 \\ & + a_2^2 \ddot{\theta}_2 + a_1 a_2 \dot{\theta}_1^2 \sin \theta_2 \\ & + g a_2 \cos(\theta_1 + \theta_2) \end{aligned}$$

$$w_{23} = 0$$

$$w_{24} = \operatorname{sgn}(\dot{\theta}_2)$$

$$w_{25} = 0$$

$$w_{26} = \dot{\theta}_2$$